

# General Conclusions

This brochure has highlighted what can be expected from numerical models regarding conductor vibrations. In the first chapter, the aeolian vibrations of single conductors are obtained using the EBP and compared with experimental results. If the range of uncertainty of the wind power functions and self-damping models which are the main input of those models is indicative of the range of uncertainty of the predicted amplitudes, then the range of uncertainty in EBP predictions of vibration amplitude is about  $\pm 50\text{--}60\%$ .

Generally, the highest vibration strains are found at relatively low frequencies, where the contribution of dampers to overall damping is much more important than that of conductor self-damping. This is not true at high frequencies. Thus, the largest deviations between models for self-damping, which occur at the lowest frequencies are less important than they may appear.

In practice, assessment of the aeolian vibration condition of particular lines, with conductors whose mechanical properties are poorly defined, or with special terrain conditions, may require field measurements. Techniques to perform such measurements have already been described [CIGRE SC22 WG11 TF2, 1995].

The same exercise has been performed on single conductors equipped with one damper at the end of the span. Benchmark results show a wide dispersion of the predicted maximum amplitude values, and large discrepancies between the analytical predictions and the measured behaviour of the test span. On the other hand, while the dispersion of the dynamic stiffness of different damper samples was reflected in corresponding dispersion in predicted amplitudes, it is not a reflection on the technology, since this dispersion will remain the same, independently of the technology used. Nevertheless, analytical methods based on the EBP and shaker-based technology can provide a useful tool for use in the design of damping systems for the protection of single conductors against aeolian vibrations. It should be used with circumspection and be supplemented by references to field experience.

The modelling of aeolian vibrations has also been evaluated for very long spans strung at relatively high tensions with multi-damper arrangements. It is more challenging since the wind velocity is not homogeneous along such long spans. Furthermore, tension at the support can be significantly greater than at mid-span due

to the large sag involved. This can cause the coupling between the vortex-induced forces and the conductor, as well as self-damping, to vary along the span.

The details of the calculation results revealed large differences in predicted clamp amplitudes among the dampers under consideration during steady vibration at a constant frequency, for most of the frequencies covered. Furthermore, these predicted clamp amplitudes were in general very different from the amplitudes on which the damper characteristics were based and, as already observed, represent one of the reasons for the discrepancies between experimental and analytical results.

Future research work is needed to improve the EBP technology, which generally produces a safe design of the damping system.

On bundles aeolian vibrations, the numerical results generally exceed the experimental ones, consequently, they are conservative, at least at low frequencies, however, the comparison was made only with a quad bundle. Other published work (Diana et al. 1976, 1982) has shown that, generally, when dealing with twin bundles, numerical results appear to be less conservative with respect to experimental data.

The sensitivity analysis demonstrated that a non-negligible influence in the assessment of conductor behaviour, when dealing with aeolian vibrations, is given by the introduction of tension differentials and variable wind turbulence with wind speed. Clearly, it is not straightforward knowing the real value to assign to the turbulence and to the tension differentials when the bundle behaviour for aeolian vibrations must be analysed.

Four models have been presented to evaluate the subspan oscillation phenomenon. FEM modelling has been applied with success but it needs a very cumbersome analysis which provides results that depend strongly on details that are not easy to quantify. Methods based on the modal analysis and energy approach seem a more useful tool for practical applications.

As previously shown experimentally, the following parameters have a predominant impact on subspan oscillation amplitudes: bundle tilt, the ratio of vertical to the horizontal frequency in each subspan, tensile load, the ratio of bundle separation over conductor diameter and subspan length. Moreover, the flow on the conductors can vary from sub-critical, critical and super-critical depending on the Reynolds number thus on the conductor diameter, wind speed and surface roughness (conventional vs. trapezoidal) and it has a paramount influence on the energy introduced by the wind.

There was only one experimental benchmark and more results are required to validate the models, however, modelling has shown that one way of controlling subspan oscillations is to increase the subspan oscillation frequency decreasing the subspan length.

This brochure has reported the state of the art regarding aeolian vibrations and subspan oscillations modelling. Of course, this field of expertise is not static and research, as much numerical than experimental, is still going on in order to improve our knowledge of the phenomenon and translate it into improved numerical models.

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