

Erratum

Fundamentals of Robotic Mechanical Systems Theory, Methods, and Algorithms Fourth Edition

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The publisher regrets the error in the print and online versions of this book. Listed below are the corrections.

Introduction: In order to ease the finding of items in this document, we have kept the page format and the original fonts of the book; we have also typeset with typewriter font--the one used in this Introduction--text that does not belong to the book.

p. 93: The correct matrix $[\mathbf{R}_2]_C$ is

$$[\mathbf{R}_2]_C = \begin{bmatrix} 0.373 & -0.926 & 0.043 \\ 0.902 & 0.352 & -0.249 \\ 0.215 & 0.132 & 0.967 \end{bmatrix}$$

p. 129: Line below Eq. (3.133a): in light of Eq. (2.39), should read: in light of Eq. (2.40)

p. 137: In Exercise 3.20, the expression for \mathbf{M}_A is faulty. The correct expression is

$$\mathbf{M}_A = \mathbf{M}_C + m\mathbf{P}\mathbf{P}^T$$

p. 144: The last line of text, “One thus has, using subscripted brackets as introduced in Sect. 2.2,”, should read:

“One thus has, using subscripted brackets as introduced in Sect. 2.3,”

The online version of the original book can be found at
<http://dx.doi.org/10.1007/978-3-319-01851-5>

- p. 171:** The third line of text below eq. (4.33), “From Definition 2.2.1, then $[u]_1 = [e7]_1 = [e6]_1$ ”, should read:

“From Definition 2.2.1, then $[u]_1 = [e_7]_1 = [e_6]_1$ ”

- p. 178:** The correct expression for Q_{123} is

$$Q_{123} = Q_1 Q_2 Q_3 = \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$[e_6]_4$ should read:

$$[e_6]_4 = (Q_1 Q_2 Q_3)^T [e_6]_1 = \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 2/3 \\ -2/3 \\ -1/3 \end{bmatrix} = \begin{bmatrix} 2/3 \\ 2/3 \\ -1/3 \end{bmatrix}$$

$\theta_{4,2}$ should be

$$\theta_{4,2} = -80.26438967^\circ$$

- p. 182:** The caption of Fig. 4.26 is faulty. The correct caption is Motoman-EA1400N welding robot: (a) top view; (b) side view; (c) orthographic projection; (d) **view A**, as per side view; (e) **view B**, as per side view. All dimensions in mm

- p. 200** Where it reads: (b) the moments of the three lines about any point on the intersecting line are all zero, the correct wording should read:

(b) the moments of the three lines with respect to the intersecting line are all zero.

- p. 202:** The expression for α is faulty. The correct expression is

$$\alpha = \frac{\sqrt{a_3^2 + b_4^2}}{\sqrt{a_2^2 + d^2} + \sqrt{a_3^2 + b_4^2}}$$

Please refer to Appendix A for details.

- p. 211:** Where it reads: with τ_a and τ_w defined as the wrist and the arm torques, respectively, the correct wording should read:

with τ_a and τ_w defined as the arm and the wrist torques, respectively.

p. 219: Equation (5.67c) should read:

$$\ddot{\theta}_1 = \ddot{\phi} - (\ddot{\theta}_2 + \ddot{\theta}_3)$$

p. 291: The second line of the expression for ι_2 should read:

$$-\frac{1}{2}m_3a_3(a_1s_{23} + 2a_2s_3)\dot{\theta}_1\dot{\theta}_3 - m_3a_2a_3s_3\dot{\theta}_2\dot{\theta}_3 - \frac{1}{2}m_3a_2a_3s_3\dot{\theta}_3^2$$

p. 321: Caption of Fig. 7.7 should read:

Mass-center location of the robot of Fig. 4.17

p. 324: The second line of the expression for $\dot{\mathbf{t}}_{11}$ should read:

$$= \begin{bmatrix} \dot{\mathbf{e}}_1 \\ \dot{\mathbf{e}}_1 \times \rho_1 + \mathbf{e}_1 \times \dot{\rho}_1 \end{bmatrix}$$

The second line of the expression for $\dot{\mathbf{t}}_{21}$ should read:

$$= \begin{bmatrix} \mathbf{0} \\ \mathbf{e}_1 \times (\omega_1 \times \mathbf{a}_1 + \omega_2 \times \rho_2) \end{bmatrix} = p \begin{bmatrix} \mathbf{0} \\ (a/2)(\mathbf{i} - 3\mathbf{j}) \end{bmatrix}$$

The fourth line of the expression for $\dot{\mathbf{t}}_{31}$ should read:

$$= p \begin{bmatrix} \mathbf{0} \\ (a/2)(\mathbf{i} - 3\mathbf{j}) \end{bmatrix}$$

The second line of the expression for $\dot{\mathbf{t}}_{32}$ should read:

$$= \begin{bmatrix} p\mathbf{e}_1 \times \mathbf{e}_2 \\ (p\mathbf{e}_1 \times \mathbf{e}_2) \times (\mathbf{a}_2 + \rho_3) + \mathbf{e}_2 \times [p(\mathbf{e}_1 + \mathbf{e}_2) \times \mathbf{a}_2 + p(\mathbf{e}_1 + \mathbf{e}_2 + \mathbf{e}_3) \times \rho_3] \end{bmatrix}$$

p. 325: Entry (3,1) of matrix $\mathbf{T}^T \mathbf{M} \dot{\mathbf{T}}$ is flawed. The correct expression for this matrix is:

$$\mathbf{T}^T \mathbf{M} \dot{\mathbf{T}} = p \begin{bmatrix} -(1/4)a^2m & (7/4)a^2m & -(1/2)a^2m - I \\ (1/4)a^2m & 0 & (1/4)a^2m + I \\ (3/4)a^2m & (1/4)a^2m - I & 0 \end{bmatrix} \equiv \bar{\mathbf{P}}$$

- p. 326:** Entries (1,3), (2,3) and (3,1) of matrix $\dot{\mathbf{I}}$ are faulty. The correct expression of the matrix is:

$$\dot{\mathbf{I}} = p \begin{bmatrix} -(1/2)a^2m & (5/4)a^2m & -I + (1/4)a^2m \\ (5/4)a^2m & 0 & (1/2)a^2m \\ -I + (1/4)a^2m & (1/2)a^2m & 0 \end{bmatrix}$$

- p. 327:** The second-to-last line of text, “Now we have”, should read:

“Now, the matrix \mathbf{C} of Coriolis and centrifugal forces is obtained as shown below:”

The last equation displayed should read:

$$\mathbf{C} = \mathbf{T}^T \mathbf{M} \dot{\mathbf{T}} + \mathbf{T}^T \mathbf{W} \mathbf{M} \mathbf{T} = p \mathbf{A}$$

- p. 328** Entry (1,1) of matrix \mathbf{A} is flawed. The correct expression is

$$\mathbf{A} \equiv \begin{bmatrix} -(1/4)a^2m & (7/4)a^2m + I & -(1/2)a^2m - 2I \\ -(1/2)a^2m - I & 0 & (1/4)a^2m + 2I \\ (3/4)a^2m + I & (1/4)a^2m - 2I & 0 \end{bmatrix}$$

The first entry of the vector array in the second equation display has a “(1/2)” too much. The correct display is

$$(\mathbf{T}^T \mathbf{M} \dot{\mathbf{T}} + \mathbf{T}^T \mathbf{W} \mathbf{M} \mathbf{T}) \dot{\boldsymbol{\theta}} = p^2 \begin{bmatrix} a^2m - I \\ -(1/4)a^2m + I \\ a^2m - I \end{bmatrix}$$

- p. 329:** The second line of the expression for $\ddot{\mathbf{c}}_3$ has an “=” too much. It should read:

$$+\boldsymbol{\omega}_3 \times (\boldsymbol{\omega}_3 \times \boldsymbol{\rho}_3) = \frac{1}{2}ap^2(-4\mathbf{j} + \mathbf{k}) - \frac{1}{2}ap^2\mathbf{j} + \frac{1}{2}ap^2(2\mathbf{i} - \mathbf{j} + \mathbf{k})$$

The expressions for \mathbf{f}_2^P , \mathbf{n}_2^P , and \mathbf{f}_1^P are faulty. They should read:

$$\begin{aligned} \mathbf{f}_2^P &= m_2 \ddot{\mathbf{c}}_2 + \mathbf{f}_3^P = \frac{1}{2}amp^2(-4\mathbf{j} + \mathbf{k}) - 2amp^2\mathbf{j} = \frac{1}{2}amp^2(-8\mathbf{j} + \mathbf{k}) \\ \mathbf{n}_2^P &= \underbrace{\mathbf{I}_2 \dot{\boldsymbol{\omega}}_2}_{Ip^2(-\mathbf{i})} + \underbrace{\boldsymbol{\omega}_2 \times \mathbf{I}_2 \boldsymbol{\omega}_2}_0 + \underbrace{\mathbf{n}_3^P}_{Ip^2(-\mathbf{i} + \mathbf{j} - \mathbf{k}) + a^2mp^2(\mathbf{i} - 2\mathbf{k})} + \underbrace{(\mathbf{a}_2 - \boldsymbol{\rho}_2) \times \mathbf{f}_3^P}_{a^2mp^2(-\mathbf{i} + \mathbf{k})} \\ &+ \underbrace{\boldsymbol{\rho}_2 \times \mathbf{f}_2^P}_{\frac{1}{4}a^2mp^2(-6\mathbf{i} - \mathbf{j} - 8\mathbf{k})} \end{aligned}$$

$$\begin{aligned}
 &= Ip^2(-2\mathbf{i} + \mathbf{j} - \mathbf{k}) + \frac{1}{4}a^2mp^2(-6\mathbf{i} - \mathbf{j} - 12\mathbf{k}) \\
 \mathbf{f}_1^P &= m_1\ddot{\mathbf{c}}_1 + \mathbf{f}_2^P = \frac{1}{2}amp^2(\mathbf{i} - \mathbf{j}) + \frac{1}{2}amp^2(-8\mathbf{j} + \mathbf{k}) \\
 &= \frac{1}{2}amp^2(\mathbf{i} - 9\mathbf{j} + \mathbf{k})
 \end{aligned}$$

p. 330: The second equation display, that of τ_1 , is faulty. The correct expression reads:

$$\tau_1 = \mathbf{n}_1^P \cdot \mathbf{e}_1 = -Ip^2 + a^2mp^2$$

The first component of vector $\mathbf{C}(\boldsymbol{\theta}, \dot{\boldsymbol{\theta}})\dot{\boldsymbol{\theta}}$ is faulty. The correct expression is

$$\mathbf{C}(\boldsymbol{\theta}, \dot{\boldsymbol{\theta}})\dot{\boldsymbol{\theta}} = \begin{bmatrix} -Ip^2 + a^2mp^2 \\ Ip^2 - (1/4)a^2mp^2 \\ -Ip^2 + a^2mp^2 \end{bmatrix}$$

Appendix A

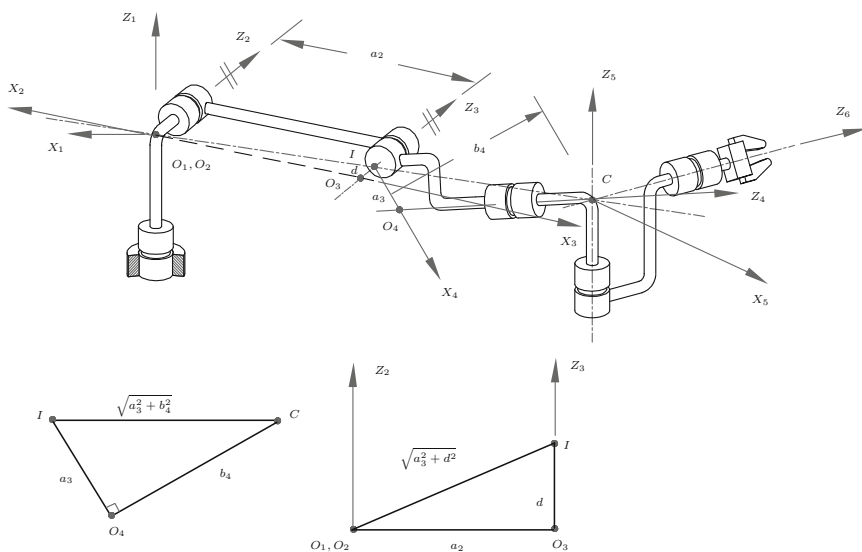


FIGURE 1. Elbow singularity of the Puma robot

With reference to the figure above, the relations below can be derived:

$$\alpha = \frac{\overline{IC}}{\overline{O_2C}} \quad (1)$$

$$\overline{IC} = \sqrt{a_3^2 + b_4^2} \quad (2)$$

$$\overline{O_2C} = \overline{O_2I} + \overline{IC} \quad (3)$$

$$\overline{O_2I} = \sqrt{a_2^2 + d^2} \quad (4)$$